EG-G B-2024





EDGERTON, GERMESHAUSEN & GRIER, INC.

FIREBALL CALCULATIONS
SHOT SANFORD
OPERATION HARDTACK PHASE II
PROJECT 15.1

DESTRICUTION STATISTICS A
Approved for public relevant
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Marie 4/25/96

REPORT NO. B - 2024 29 JANUARY 1960 BOSTON, MASSACHUSETTS • LAS VEGAS, NEVADA
SANTA BARBARA, CALIFORNIA



Defense Nuclear Agency 6801 Telegraph Road Alexandria, Virginia 22310-3398



ISST

29 May 1996

MEMORANDUM FOR DEFENSE TECHNICAL INFORMATION CENTER ATTENTION: OCD/Mr. Bill Bush

SUBJECT: Documents for DTIC System

There is no record of your office receiving the following reports:

EGG-B-2024 (29 January 1960) Fireball Calculations Shot Sanford Operation Hardtack Phase II Project 15.1

EGG-B-2013 (29 January 1960) Fireball Calculations Shot Hamilton Operation Hardtack Phase II Project 15.1

Both documents are now approved for public release.

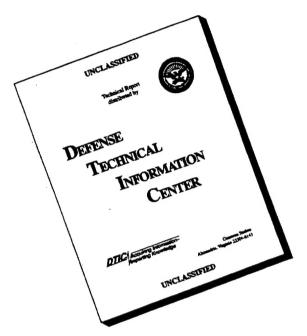
Therefore, we are transmitting copies for inclusions into the DTIC system, if not already there.

Enclosure: A/S

ARDITH JARRETT
Chief, Technical Support

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FIREBALL CALCULATIONS

SHOT SANFORD

OPERATION HARDTACK, PHASE II

PROJECT 15.1

Report No. B-2024 29 January 1960

Prepared by Landy

J. E. Campbell

Approved by

D F Seacord Jr

EDGERTON, GERMESHAUSEN & GRIER, INC.
Boston, Mass. Santa Barbara, Calif. Las Vegas, Nev.

FIREBALL CALCULATIONS: SHOT SANFORD

1.0 INTRODUCTION

Sanford, an LRL event, was detonated on 26 October, 1958, at approximately 0220, PST, from a 1500-foot balloon in Area B-Fa of the Nevada Test Site. The fireball yield was 4.89 kt ± 0.30 kt.

2.0 CAMERA INSTRUMENTATION AND OPERATION (Table I)

Photographic coverage of fireball growth was provided by four-high-speed Eastman cameras, two each at Stations F-362 (6 x 6 No. 2) and F-369 (6 x 6 No. 3). In addition, Rapatronic cameras were located at each of these stations to record early fireball phenomena. All cameras functioned properly and provided records suitable for analysis.

The station and burst locations are shown in Fig. 1. Figure 2 contains the survey data.

3.0 RESULTS

Application of \emptyset scaling to the Sanford data indicates a yield of 4.89 kt \pm 0.30 kt.

An air density of 1.062 grams per liter was used in the yield calculations. This air density was based on a pressure of 864 millibars, a temperature of 9.4°C, and a relative humidity of 78 percent at the height of the device at shot time. Diameter vs time and phi vs time plots are given in Figs. 3 and 4. Table II shows average diameter vs time.

The zero-frame times of the Eastman cameras were determined by comparison with the Rapatronic diameter vs time data.

The following data sheets are included for each shot:

- (a) Photo Plan and Photo Loading Chart
- (b) Camera Data and Calculation Sheet
- (c) Diameter Measurement Sheet
- (d) E102 print-out sheet of D, t, \emptyset and W (yield).

The Appendix contains photographic examples of the Sanford Fireball.

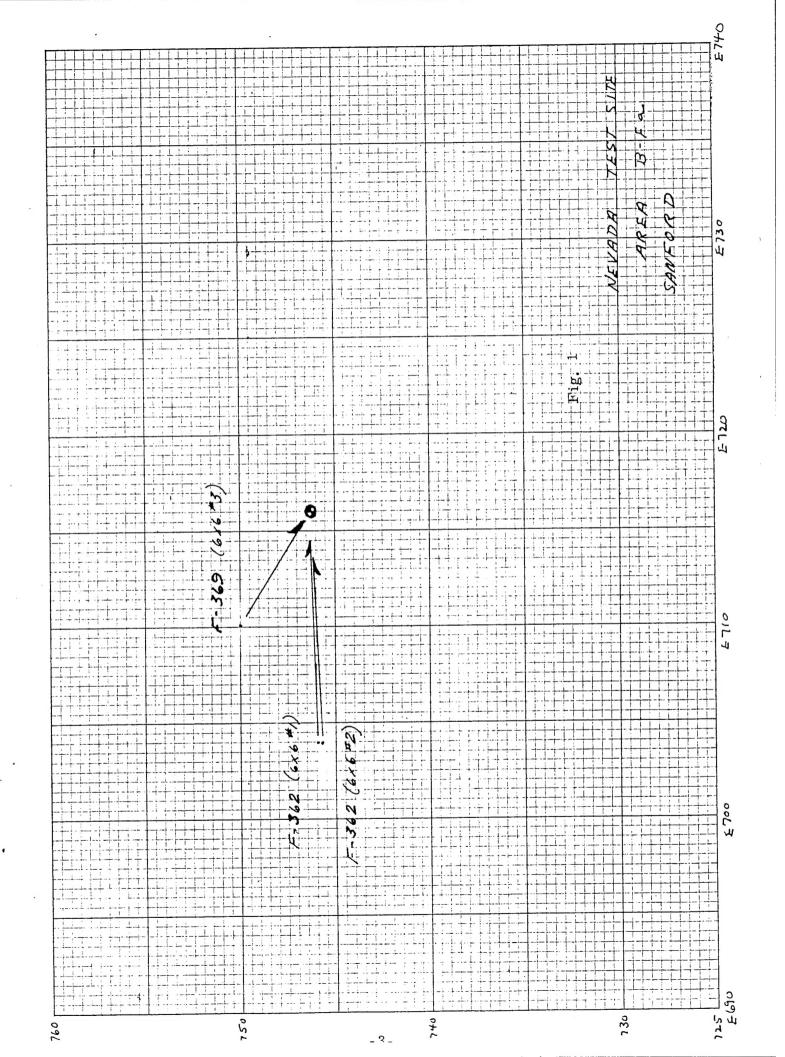


Fig. 2

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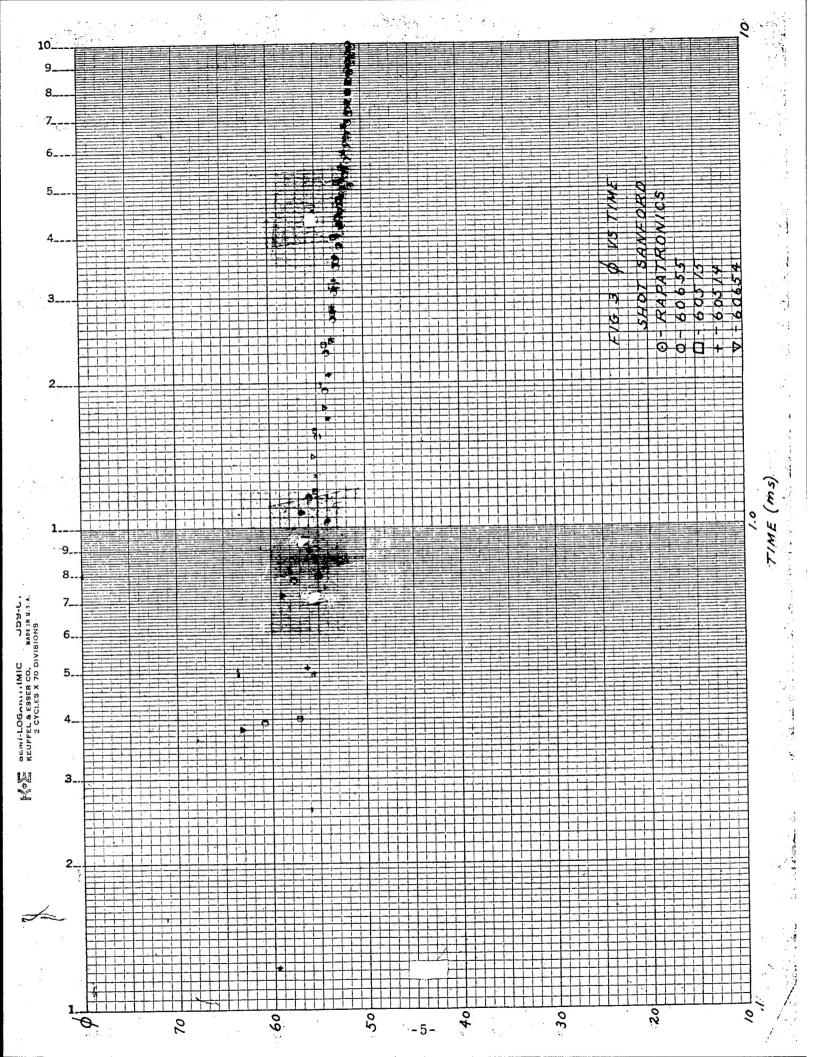


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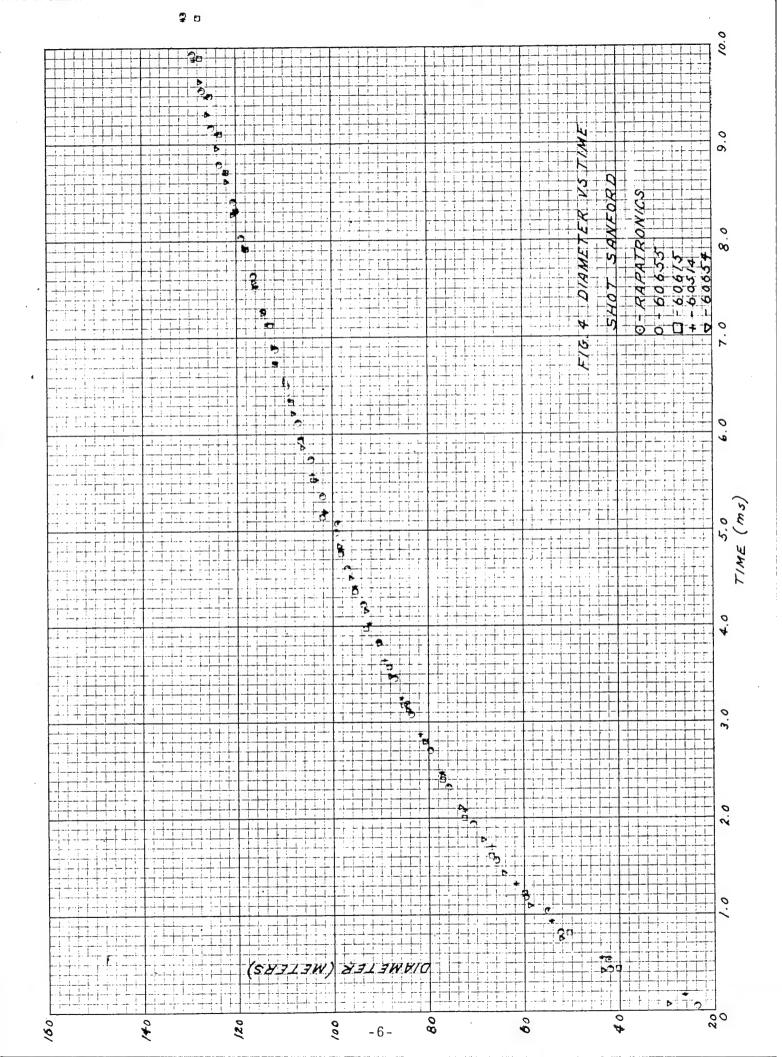


Table I

Hardtack Phase II, Sanford

Fireball Camera Distribution

Station	Camera	Qualitative Functioning
F-362 (6 x 6 No. 2)	E-34	Record
	E-7	Record
	R-30	Record
	R-34	Record
		•
F-369 (6 x 6 No. 3)	E-25	Record
	E-6	Record
	XR-3	Record
	R-4	Record

Table II

Hardtack Phase II, Sanford

Average Diameter vs Time

Time (in msec.)	Diameter (meters) as seen from Stations 7-357 and 9-356	
0.5	43.0	
1.0	57.0	
1.5	65.5	
2 .0	71.5	
2 .5	78.5	
3.0	83.0	
3.5	87.5	
4.0	92.0	
4.5	96.0	
5.0	100.0	
5. 5	103.5	
6.0	106.5	
6. 5	110.0	
7.0	113.0	
7.5	116.0	

Table II, contid

Time (in msec.)	Diameter (meters) as seen from Stations 7-357 and 9-356
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8.0	119.0
8. 5	121.5
9. 0	124.5
9. 5	127.0
1 0. 5	129. 5

Table III

Hardtack Phase II, Sanford

Rapatronic Summary

	Station	Film No.	Camera No.	Range (m)	F. L. (mm)	F. L. (mm) Diameter (m) Time (msec)	Time (msec)
	F-362 (6 × 6 No. 2)	60665	R-30	3704.1	. 479, 30	41.90	0,489
-10-		99909	R-34	3704.1	479,03	84.03	3, 182
	F-369	60658	R-4	2196.3	482, 35	98.46	5, 09
		60657	·XR-3	2196.3	476,76	54.57	1,02

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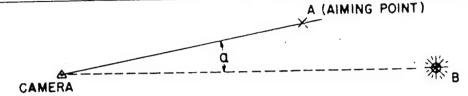
FORM E-40

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TATION NO.	TATION TYPE 6 X6 3	SISTANCE OBJECT
1	F. S.	Ä

CAMPERA CAMP	NOM RACK FOC. S/N FILTER H/V OBJECT H V VOLTS RHEO. ON/OFF	DELAY FILM	POSE
9500 B-2 63 ET 207 W-12 1265 GB 000 12 12000 190 -155 00 101 == ME 18.1 9500 B-2 63 ET 207 W-12 1265 GB 000 12 12000 190 -155 00 14 == ME 18.1 9500 B-2 185 815762 W-12 1265 GB 000 15 12000 170 -155 00 14 == ME 18.1 900 B-2 185 815762 W-12 1253 GB 000 15 12000 170 -157 00 101 == TRIX 15.1 900 B-2 185 815762 W-12 1253 GB 000 15 125 00 101 == TRIX 15.1 900 B-2 185 815762 W-12 1253 GB 000 15 125 00 101 == TRIX 15.1 900 B-2 185 815762 W-12 1253 GB 000 15 125 00 101 == TRIX 15.1 900 B-2 185 815762 W-12 1253 GB 000 15 125 00 101 == TRIX 15.1 900 B-2 185 815762 W-12 1253 GB 000 15 125 00 101 == TRIX 15.1 900 B-2 185 815762 W-12 1253 GB 000 15 125 00 101 == TRIX 15.1 900 B-2 185 815762 W-12 1253 GB 000 15 125 00 101 == TRIX 15.1 900 B-2 185 815762 W-12 1253 GB 000 100 100 100 100 100 100 100 100 10	\$\frac{\text{spb}}{2500}\$ \text{Pos}\$. \text{MM}\$ \text{NO-1} \cdots \cdots \text{Vod} \text{For}\$ \text{Vod} \text{For}\$ \text{Vod} \text{For}\$ \text{Vod} \text{For}\$ \text{Vod} \text{Vod} \text{Vod} \text{Vod} \text{Vod} \text{Vod} \text{Vod} \text{Vod} \text{Vod} \text{Vod} \text{Vod} \text{Vod} \text{Vod} \text{Vod} \text{Vod} \text{Vod} \text{Vod} \text{Vod} \qua	TYPE S/N MS	
3500 B-2 63 ET 1207 W-10 304 6.8 000 12 1200 14 = ME 15.1 3500 B-3 40 3332516 W-12 1500 6.8 000 15 1000 10 1 = TRIX 15.1 3500 B-3 40 3332516 W-12 1500 6.0 00 150 1000 10 0 0 0 14 5.1 3500 B-3 18.5 35572 W-12 1500 6.0 00 150 1000 10 0 0 0 14 5.1 3500 B-3 18.5 35572 W-12 1500 6.0 00 150 1000 10 0 0 0 14 5.1 3500 B-1 480 723150 = 753 6.0 00 10 10 10 10 10 10 10 10 10 10 10 10	2500 A-2 63 ET 1207 W-13 804 F.B. 000 12 1200C 80 11.55 2500 A-3 40 3332516 W-12 1.265 100 B-2 18.5 36516 W-12 1.265 100 B-3 18.5 36516 W-12 1.265 100 B-3 18.5 36517 W-13 1.265 100 B-3 18.5 18.5 18.5 18.5 18.5 18.5 18.5 18.5	101 000	1.5.1
2500 B-3 4/0 3032518 WO-12 1265 163. 000 12 12000 170 - 5/30 200 101 = 701 15.1 C3Y 100 B-3 18.5 365162 WO-12 1265 163. 000 120 3/5 84.8 = 5.41 26 100 0 0 0 1/5 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2500 A-3 40 3232516 W-72 1,263 F.B. 000 17 19000 80 F.730 100 B-2 18 5 345767 W-12 7330 6200 000 1705 12000 170 1730 4445 A-1 480 774555 = 753 F.B. 000 120 1758	JA = ME	5.1
Pob B.3 18.5 345767 W-13 7330 64040 2000 70 75	100 B.2 18.5 365767 W-12 7330 CLOUD 000 1805 12006 1700 1730 4445 H-1 480 773150 = .753 F.B. 000 12 34bc Bulb 601 B.3 9.5 255 = .753 F.B. 000 12 34bc Bulb 644 B.3 9.5 255 = .755 Doc. 000 13 34bc 133 130 644 B.3 9.5 255373 = 5.350 Doc. 000 1565 24bc 133 130 7.9000 7.900 7.900 7.900 7.900 7.900 7.900 7.900 7.900 7.90000 7.	200, 101 = TRIX	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	444.5 A-1 480 773150 = .753 FB 000 12 34BC BULB = .753 FB 000 12 34BC 133 750 FB 153	EN 21 1000 PP	Can 1
10	4945 B-1 480 773350 = .753 F.B. 000 12 240C BULR 64 R.3 9.5 255219 = .7530 DOC. 000 15/15 240C 133 730 64 B-3 9.5 255219 = .5350 DOC. 000 15/15 240C 133 730 64 B-3 9.5 255219 = .5350 DOC. 000 15/15 240C 133 730 7907444 DOC 100 15/15 240C 133 730 7907444 DOC 100 15/15 240C 133 730 790744 DOC 100 15/15 240C 133 730 79074 DOC 100 15/15 240C 133 740C 133 740C 133 743C 79074 DOC 100 15/15 240C 79074 DOC 1	26 5000	Can #
64 8-3 9.5 205219 = 5.350 DOC. 600 51 2400 133 / 130 = = D C	64 B-3 9.5 2559.9 - 5.350 DOC. 000 15.15 24D0 133 130 -5 130 64 B-3 9.5 255319 - 5.350 DOC 000 50.5 34D0 133 130 -5 130 7.750 DOC 000 50.5 34D0 133 130 -5 130 7.750 DOC 000 50.5 34D0 133 130 -5 130 7.750 DOC 000 50.5 34D0 133 130 -5 130 7.750 DOC 000 50.5 34D0 133 130 -5 130 7.750 DOC 000 50.5 34D0 133 133 130 7.750 DOC 000 50.5 34D0 133 130 7.750 DOC 000 50.5 3	*	/5: /
64 B-3 9.5 25319 = 5.350 DDC 000 508 3400 133 730 NARKS NARKS NARKS NACHAGES 1500 4th height of bellown	64 8-3 9.5 25529 = 7.75 DOC 000 1515 3400. 133 1130		12.1
AARKS AA	70 DELBYS 18-3 10127 WS 18-4 5073.1 WS		
10197 425 hot 6 1 delcy 1 2 45 hot 6 1 delcy 10197 455 + 24 45 hot 6 1 delcy 10197 455 + 24 45 hot 6 1019 1019 1019 1019 1019 1019 1019 10	TURL ARP DELRYS XR-3 (013,7 445) R-4 5023.1 45		
1013 1 2 45 45 1013 1 45 4 2 45 40 1 669. (4405 1500 ft, hought of bolloon	XR-3 (1017) 445 R-4 5023.1 45		
1017.7 445 42 45 45 445 45 45 46 66; 10 10 10 10 10 10 10 10 10 10 10 10 10	3 1017.7 445	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	1
1, des 1500 ft. height of belloon	5003.1 4S	7 2 K	30
(4) des 1500 tt. height of belloon		+	7
ludes 1500 ft. height of belloon			
	(udes 1500 ft. height of bello		
			FINAL

OPERATION: HARDTACK PHASE II CAMERA DATA & CALCULATIONS

FILM NO. 60655	f STOP	CAMERA NO. E-6	CALCULATED BY: JEC
STATION NO. 6 x 6 #3	EQ. AP.	LENS TYPE	DATE: 12/1/58
RACK POS.	ND	LENS NO. 3232586	
TEST SANFORD	COLOR FILTER:	β=EL. ANGLE	



HORIZONTAL PROJECTION

A. $R ^{\circ}/A = CB_h \cos \alpha \cos$	$\beta + (H_B - H_C) \sin \beta$	
a= 0° 00'	β= /2°	H _B = 4577 ft
cos a = /. 0000	$\cos \beta = 0.97815$	H _C = 3078 ft
$CB_h = 2/48.2 m$	$\sin \beta = 0.2079/$	$\Delta H = /499 ft = 456.9 m$
CB _h cos α cos β = 2/0/.3 m	$\Delta H \sin \beta = 94.99 m$	$R^{0}/_{A} = 2/96.3 m$
B. FOCAL LENGTH 39.		

C. MAGNIFICATION FACTOR (meters/in.) /396.5

D. ZERO TIME CORRECTION 0.01 ms

NFORD

FILM NO. 60655 Z-6

	02				FLEXOWR	NUMBER
Mag.	D ₁	D2,	D ₃	Dave (m)	Deve (m)	t (ms)
48.15	0079 0145 0179 0206 0227 0244 0261 0273 0387 0300 0311 0323 0334 0343 0210 0215 0226 0231 0246 0251 0255 0255 0263 0270 0272	0262 0267 0271 0274		23.35 41.76 52.06 59.31 65.54 70.33 75.40 79.17 83.23 86.71 90.05 93.38 96.57 99.04 101.47 103.89 106.55 108.96 111.38 114.04 115.97 114.04 115.97 114.63 120.32 124.91 126.64 128.77 131.91 133.36		
	RH	GG)		TYPED BY	
		11/5/58	3		DATE	

EDGERTON, GERMESHAUSEN & GRIER, INC.

FIREBALL CALCULATIONS

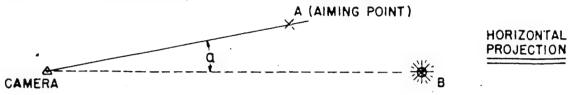
SHOT <u>SANFORD</u> FILM NO. <u>60655</u>

DATE <u>11/5/58</u>

D	· •	In D	Int	+ ² /5	ф	W
23.35	.01	3.150 F3	4,60509 -	.1 59064	1 4 <i>6.</i> 7 95	920,909
4176	39	3 732 01	04153 -	6 861 80	608 58	11278
5206	77	3 9 5 2 3 8	26135 -	900735	57797	3713
59 31	115	408271	13968	1057464	56086	7498
65 54	1 54	418259	431 85	1188560	551 42	68 87
7033	1 92	425315	65233	1298144	54177	× 63.05
7540	2 30	4 322 80	832.84	1395338	54037	6224
7917	269	4 371 63	98947	1485556	532 93	5807
83 23	307	4 4 2 1 67	112166	1566219	531 40	57 25
8671	345	446265	1 238 41	1641099	52836	55 63
9,005	3.83	4 500 44	1 342 93	1711166	526 24	5452
9338	4 22	4 536 73	1 4 3 9 9 0	1778843	52494	5385
9657	₂ 4 60	457027	1 52 <i>6</i> 10	1841244	52448	53 61
9904	4 98	4 595 47	160543	1900611	521 09	51 90
10147	5 36	461980	1 678 93	1957314	51841	50 58
10389	5 75	464332	174913	20 1 3 0 5 9	51608	4945
106 55	613	4 668 56	181311	20 652 41	51592	4938
10896	6 F1	4 690 91.	· 187326	21,15530	51504	4896
111 78	6 29	471287	1 9 3 0 0 1	21 641 01	51467	4878
11404	7 28	473647	1 985 10	2212317	51547	4917
11597	766	4 753 25	203601	22 578 36	51363	48 29
118 63	804	477594	208447	23 020 21	51532	4909
12032	842	4 790 09	213067	23 4 4 9 6 5	51309	48.04
12322	8 5 1	481392	217596	23 878 31	51603	4943
12491	919	4 827 55	221817	2428494	51 4 35	48 63
126.84	9 5 7	484288	2 2 5 8 6 5	24 681 28	51391	4842
12877	9 9 5	4 8 5 8 0 1	2 2 9 7 5 0	25 067 89	51368	48 32
13071	1033	4 872 97	2 3 3 5 0 5	25 4 4 7 2 4	51365	4830
13191	1072	4 882 12.	237206	25 826 73	51074	4 <i>E</i> 95
13336	1110	4 893 06	240687	26 188 87	509 22	46 25

OPERATION: HARDTACK PHASE III. CAMERA DATA & CALCULATIONS

FILM NO. 60514	f STOP		CAMERA NO. E-34	CALCULATED BY
STATION NO. F-362	EQ. AP.		LENS TYPE	DATE: /2/1/58
RACK POS.	ND	;	LENS NO. ET-1254	
TEST SANFORD	COLOR FILTER:		β=EL. ANGLE	



A. $R^{\circ}/A = CB_h \cos \alpha \cos \beta + (H_B - H_C) \sin \beta$				
a= 0°00′	β= 7° 02'	H _B = 4577 f+		
cos a = /. 0000	$\cos \beta = 0.99.248$	H _C = 3090 f+		
	$\sin \beta = 0. /2245$	ΔH= 1487 ft = 453.		
$CB_h \cos \alpha \cos \beta = 3648.6m$	$\Delta H \sin \beta = 55.49 m$	R ⁰ /A= [3704.1m		
B. FOCAL LENGTH 63	3.91 mm (ET-1254)			

C. MAGNIFICATION FACTOR (meters/in.) /472./

D. ZERO TIME CORRECTION 0.12 ms

FILM NO.E-34 F-362

60514

0 48.15 0083 12 0142 2 0171 3 0206 4 0216 5 0245 7 0261 8 0276 9 0285 10 0306 11 0316 12 0326 13 0336 14 0336 15 0347 16 28.90 0214 17 0215 18 0222 19 0226 20 0233 21 0234 22 0246 23 0247 25 0257				
12 0142 2 0171 3 0200 4 0216 5 0235 6 0245 7 0261 8 0278 9 0285 10 0300 11 0310 12 0320 13 0330 14 0330 15 0347 16 28.90 0211 17 0215 18 0222 18 0224 29 0234 21 0234 22 0246 25 025	D ₂	exowri (m) xx	Dave D	t (ms)
	0140 0177 0200 0218 0235 0252 0266 0278 0291 0301 0310 0320 0331 0346 0211 0218 0222 0227 0230 0235 0247 0251		25.53 43.10 53.65 61.14 66.34 71.84 76.58 81.01 84.98 88.65 91.86 94.77 97.82 101.03 103.63 105.93 108.25 111.30 113.09 113.09 117.67 119.45 121.75 123.78 125.82 125.82 130.66	
READ BY GGO	JEC	ť	TYP	
DATE 11-5-	8	·	DATE	

REMARKS:

FIREBALL CALCULATIONS

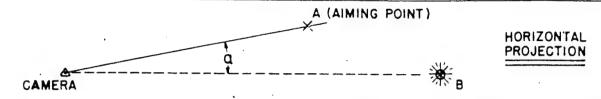
SHOT <u>SANFORD</u> FILM NO. <u>605/4</u>

DATE <u>II/5/58</u>

D.	t	In D	Int	t ^{2/5}	ф	W
25.105444818556723335098755827 25.10544488185672333509875582583 1112258	121098765543210987654322109 1122223344455556677788999	3.763 259 3.763 259 3.763 269 3.763 269 3.763 269 3.763 269 4.194 4.49 4.194 4.49 4.194 4.49 4.194 4.19 4.194 4.19 4.194 4.19 4.194 4.19 4.194 4.19 4.194 4.19	2.127535 105359 1054685 2548858 1054862 1075187 10778 10788 10788 10788 10788 10788 10788 10788 10788 10788 10788 10788 10788 1088 10	4 282 14 7 638 92 9 587 58 11 072 18 12 307 77 15 377 77 15 023 43 16 766 84 17 463 66 18 744 02 19 337 43 19 90 448 80 20 97 6 42 20 97 6 42 21 964 20 22 436 63 23 337 79 24 60 97 24 60 97 25 00 7	19279 19279	1721369303820599799089652995077493438082059979908965299508844447771866688555555554544444444444444444444444
13066	1028	4 872 59	2 330 21	25 398 00	51444	48 6 <u>8</u>

OPERATION: <u>HARDTACK PHASE II</u> CAMERA DATA & CALCULATIONS

FILM NO. 60515	f STOP	CAMERA NO. E-7	CALCULATED BY: DB
STATION NO. 6 × 6 #2	EQ. AP.	LENS TYPE	DATE: 10/26/58
RACK POS.	N D	LENS NO. RC 486	
TEST SANFORD	COLOR FILTER:	β=EL. ANGLE	



A. $R \% = CB_h \cos a \cos b$	$\beta + (H_B - H_C) \sin \beta$	
a = 0° 00'	β= +7° 02'	H _B = 4577ft
COS a = 1.0000	$\cos \beta = 0.9925$	H _C = 3090 ft
CBh = 3676.2 m ;	$\sin \beta = 0.1224$	ΔH = /487 ft = 453.2 m
$CB_h \cos a \cos \beta = 3648.6 m$	$\Delta H \sin \beta = 55.47 m$	$R^{0}/_{A} = [3704.1 m]$
B. FOCAL LENGTH 633	93 mm (RC 486)	

C.	MAGNIFICATION	FACTOR	(meters/in.) 50.73

D. ZERO TIME CORRECTION 0.40 ms

E-7 F 362
FILM NO. 60515

Pr. No.	Mag.	בת	D ⁵	D3	Dave (m)	D (E)	t (25)
0 12 34 56 78 90 11 12 13 14 156 17 18 19 20 12 21 22 22 22 22 26 27	29.00	0078 0099 0117 0131 0142 0150 0157 0167 0167 0186 0194 0200 0205 0209 0213 0220 0222 0228 0236 0240 0249 0252 0246	0098 0117 0130 0141 0151 0158 0167 0173 0181 0199 0203 0213 0208 0213 0221 0236 0240 0243 0247 0252 0256 0258		39.58 50.23 51.39 66.49 72.05 76.62 80.11 84.74 87.78 92.35 94.88 97.93 101.48 103.51 106.05 108.08 111.63 112.64 117.72 119.75 121.78 123.30 125.33 127.36 130.91 132.94		
READ BY		GGO	JEC			TYPED BY	
ATE		10.	/26/58		1	DATE	

REMARKS:

FIREBALL CALCULATIONS

SHOT SANFORD	FILM NO. 605/5
	DATE

D .	†	In D	Int	t ² /5	ф	W
77 FO		7 475 40		1074.6A	77100	22.60
39,58 50,23	.40 .70	3,47940 3,91672	.018 (1) H .778 6 F F	.6 93 1 64 910028	57100 58196	5,2 00, 69 21
50 77	1 19	408372	17388	1072030	53.50	7038
6847	159	419668	46381	1203849	55214	6933
72.05	1 98	4 277 33	68309	1314212	54823	66 91
76.62	238	4 338 86	86702	1414548	541 65	6299
8017	278	4 38419	1 022 39	1505247	53260	57.89
8474	317	4 4 3 9 6 6	1 1 5 3 7 3	1586440	53415	5974
9773	3 57	447491	1 272 62	1663707	527 61	55.23
9235	3 97	4 525 65	1 378 84	1735919	531 99	57 na
្នែកទ	436	4 552 64	1 472 53	1902213	52646	5443
9703	4 76	4 584 23	1 560 28	18 665 87	52464	9.3.70
10148	5 1 5	461990	1 638 98	1926288	526.81	နည်း မြော
10351	5.55	4 639 66	171375	1984764	521 52	-21 <u>2</u>
10005	5 O.5	466327	1 783 32	20 40771	51965	51:9
10-08	634	4 682.21	184680	20 932 55 °	51632	49.57
11153	€ 74	471511	1 907 99	21 451 23	520.78	
11254	714	472411	1 965 67	21 951 90	51318	4805
11559	7 53	4 750 93	201888	2242419	51591	. 4937
11772	7.93	4 768 23	2 0 7 0 6 8	2289363	51.4.20	48 FM
110.75	535	478534	211872	23 337 79	51311	4875
12174	9.72	480216	216569	23 780 43	51210	47 18
127 50	911	4 81 4 57	220944	24 200 20	50949	46 32
10033	951	4 830 01	2 2 5 2 3 7	2461936	50907	46.18
12736	0.01	484600	2 293 49	25 027 64	508.87	45 1 <u>0</u>
125 36	1030	4.850.91	2 332 15	25 417 71	50303	43 51
43501	1070	4.874.50	0.37019	25,807,44	50745	45.37
13504	1100	9 8 3 Q 0 O	240537	26:179:43	50750	4561

OPERATION: HARDTACK PHASE II

CH M NO 1			
FILM NO. 60654	f STOP	CAMERA NO. E-25	CALCULATED BY: JEC
STATION NO. F-369	F0 15		STEEDERIED DITOZE
STATION NO. 6x6 #3	EQ. AP.	LENS TYPE	DATE: 12/1/58
RACK POS.	NS		DAIL: 12/1/38
MAUN FUS.	ND	LENS NO. ET-1207	
TEST SANFORD	COLOR FUTER		
ILSI SANFORD	COLOR FILTER:	β =EL. ANGLE	
			l .

A (AIMING POINT)

HORIZONTAL PROJECTION

A. $R^{\circ}/A = CB_h \cos \alpha \cos \alpha$	$\beta + (H_B - H_C) \sin \beta$	
a= 0°00'	β= /2°	H _B = 4577f+
$\cos \alpha = /.0000$	$\cos \beta = 0.978/5$	H _C = 3078 ft
$CB_h = 2/48.2 m$	$\sin \beta = 0.2079/$	$\Delta H = 1499 ft = 456.9 m$
CBh cos α cos $\beta = 2/0/.3 m$	$\Delta H \sin \beta = 94.99 m$	$R^{0}/_{A} = 2/96.3 m$
B. FOCAL LENGTH 64	.10 mm. (ET-1207)	

- C. MAGNIFICATION FACTOR (meters/in.) 870.28
- D. ZERO TIME CORRECTION 0.03 ms

DIAMETER MEASUREMENTS

SHOT	Sanford	~			E- FILM NO		STA-369
Fr. No.	Mag.	D ₁	D _S	D ₃	D _{avg}	PLEXON Dave (m)	RITTER t (ms)
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 22 24 26 7 28	48.15, 28.90	0236 0353 0353 0254 0254 0267 0299 0318 0335 0335 0335 0344 0256 0269 0269 0274 0282	0161 0240 0286 0324 0353 0226 0242 0255 0266 0279 0298 0307 0318 0327 0335 0242 0248 0248 0248 0266 0266 0269 0273 0281		29.00 43.01 51.77 58.37 63.79 68.05 73.02 76.63 80.24 83.86 87.47 89.88 92.59 95.75 98.31 100.87 102.98 105.68 107.72 109.53 112.02 114.06 116.09 118.13 120.39 121.75 123.79 125.82 127.44		
READ BY			rh		TY	PED BY	
DATE		11-5-58					

REMARKS:

DATE

FIREBALL CALCULATIONS

SHOT <u>SANFORD</u>. FILM NO. <u>60654</u>

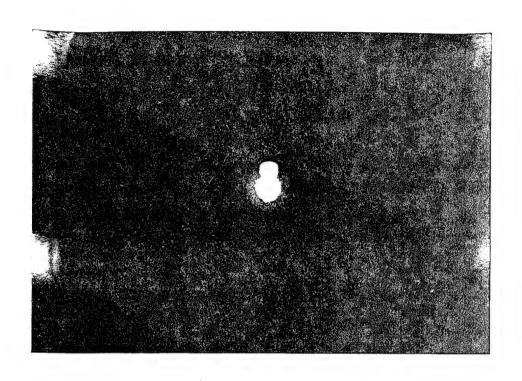
DATE <u>11/5/58</u>

D	† · · · · · · · · · · · · · · · · · · ·	In D	Int	t ² /5	ф	w
29,10	.13	3,36725	3.506 56 ×	.2 4 5 9 9 9	1 17.8 86	. 307 . 589
4301	7.8	3.761 50	967 51 -	6 7 90 86	63335	13768
51 77	25	304880	₹28 °4 ~	a 768 5 <u>1</u>	5,9040 .	9692
5837	1 07	4,066.74	1 67 60	1027412	56812	79 96
6379	1 41	4 1 55 52	34363	11 473 48	55597	7175
FROF	176	4 22018	56537	12 537 61	54276	€3,63
7302	210	429071	74190	13 454 94	54269	63.59
75.63	214	4 33900	891 92	1428704	536 35	59.97
≥0.04	279	4 38506	1 025 98	1507411	532 30	57.73
83.86	313	442921	114102	15 783 99	531 29	5719
27.47	3 48	447137	124707	1646795	53115	5711
3000	382	4 4 9 8 5 5	134032	1709377	525.80	5429
0259	- 416	4 522 24	1 425 59	1769684	52349	53.11
0575	4 51	4 561 75	1 50 <i>6</i> 35	1926754	52415	57.45
32 3 <u>1</u>	4 8 5	4 58809	1 579 00	1980618	52275	52.74
10097	5.20	4 613 88	1 648 64	1933743	52163	5217
402.03	5 = 4	A 634 54	1 711 94	1983334	51922	50.98
10568	5 28	4.660.38	1 771 48	20 311 36	52029	51 51
10772	೯ 23	467947	1 829 29	20 78 <i>6</i> 51	F18 22	5049
10953	€ 57	4 696 13	1 882 44	21 233 09	51584	4934
12005	€ 91	471960	1 932 91	21 666 12	51702	49 01
11406	726	4 736 64	1 982 34	22 098 8 3	51613	4948
11509	7.60	4 754 29	202814	22 507 41	51578	4931
4 # 0 1 3	7.95	4 771 71	207320	2291672	51547	4915
12039	8 29	4 790 67	211510	2330408	51 <i>6</i> 60	49.71
18175	e 63	4 801 91	215531	23 681 93	51410	4251
12779 .	୍ ବ ପଥ	1 21 2 54	210507	24 061 53	F1447	48 69
12502	033	187161	9.038.81	24431 56	51519	49.03
127/11	3.56	3 947 79	22€739	2477371	51429	4 8 6 <u>0</u>

APPENDIX

SHOT SANFORD

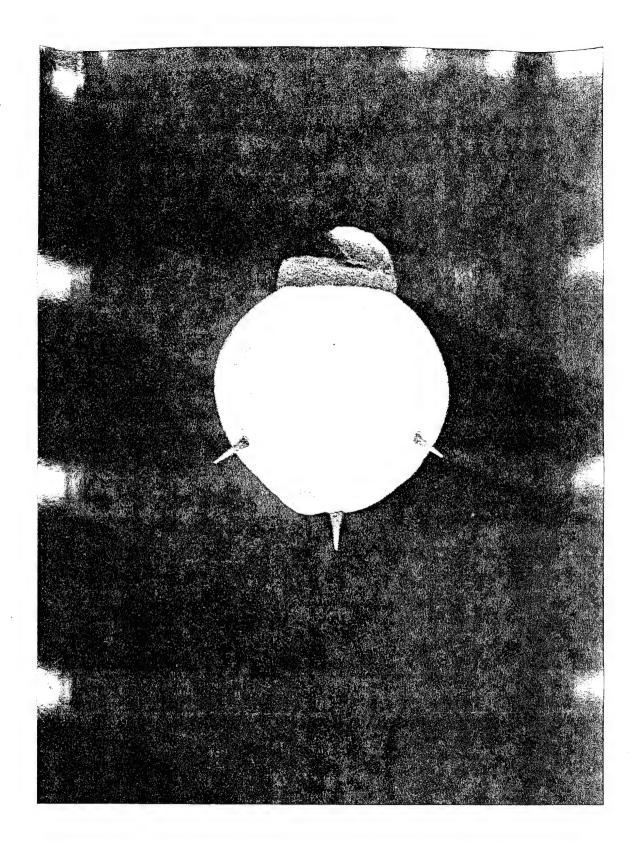
PHOTOGRAPHIC EXAMPLES



Camera: E-34

Station: F-362 (6 x 6 No. 2)

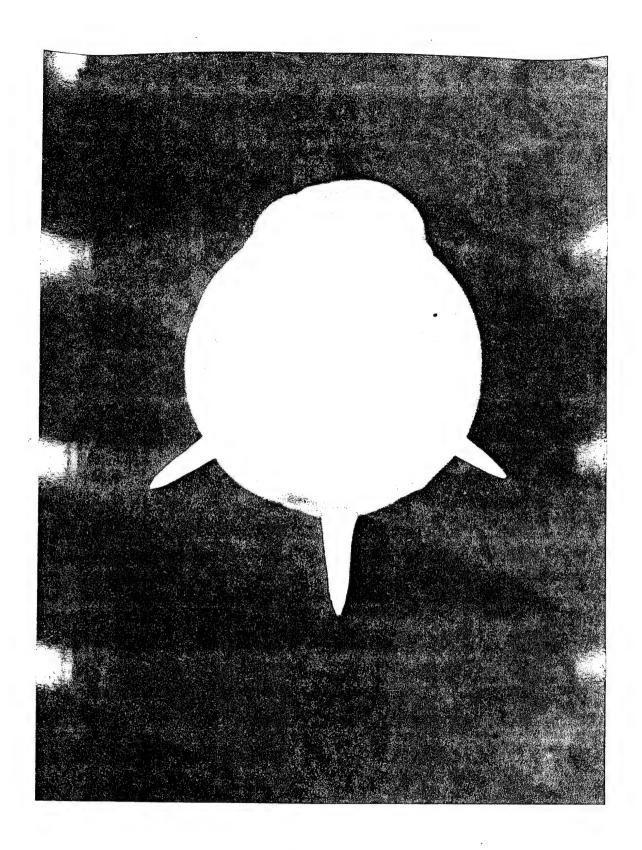
Time: .12 msec



Camera: R-30

Station: $F-362 (6 \times 6 \text{ No. 2})$

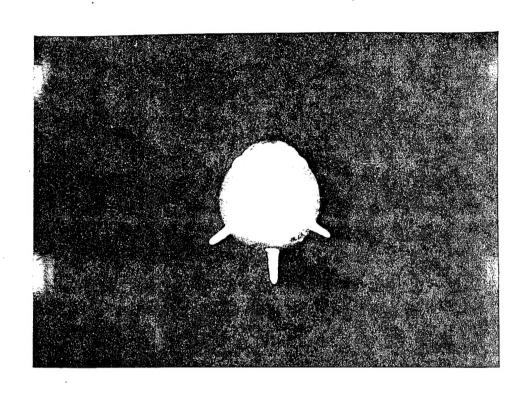
Time: 0.49 msec



Camera: R-34

Station: F-362 (6 x 6 No. 2)

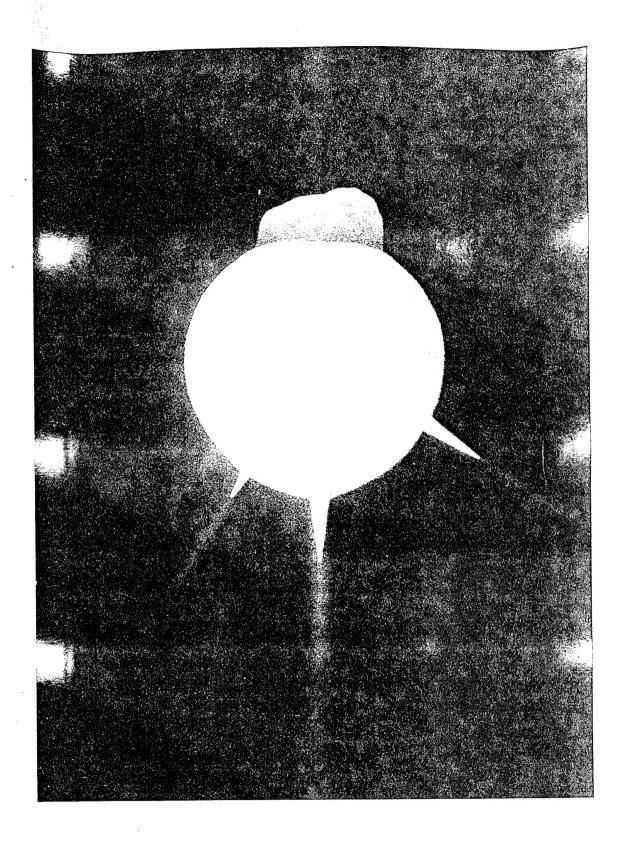
Time: 3.18 msec



Camera: E-34

Station: F-362 (6 x 6 No. 2)

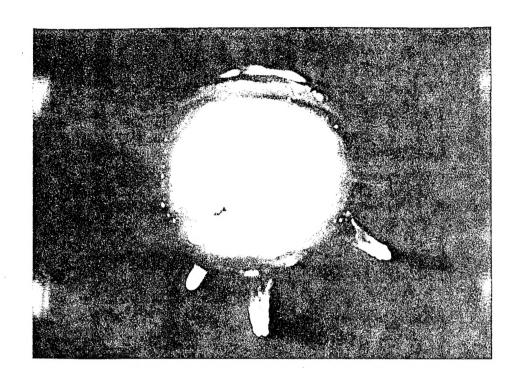
Time: 6.37 msec



Camera: XR-3

Station: F-369 (6 x 6 No. 3)

Time: 1.02 msec



Camera: E-25

Station: $F-369 (6 \times 6 \text{ No. 3})$

Time: 10.01 msec

Distribution

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